



The
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EXAMPLE COMPARISON OF 1584-2002 AND 1584-2018 INCIDENT ENERGY CALCULATIONS

1.0 INTRODUCTION

The IEEE Guide for Performing Arc-Flash Hazard Calculations was first published in 2002. It was a ground-breaking document that provided guidance to the industry for making arc flash calculations. The publication of that document also set in motion a significant testing project to expand our knowledge base in this area. Based on this work, the standard was updated in 2018. One of the significant variables, which was investigated since 2002, included the placement of the three electrodes (or phases). In Figures 1 and 2, the variation of the phases is illustrated.

In Figure 1, a vertical arrangement of the three phases is illustrated with an arc flash at the bottom of the electrodes. There can be a significant difference in the heat that is expelled out the open front of the enclosure, depending upon how open the area is where the arc occurs. The configuration on the left is labeled as VCB with the electrodes in a vertical position and an open space at the bottom of the electrodes. The configuration at the right is labeled as VCBB with the electrodes also in a vertical position but with very little open space at the bottom. The VCBB configuration generally results in more heat being expelled out the front opening toward the person. It should be noted that the testing which produced the 2002 document was predominantly done with configurations that were similar to VCB.

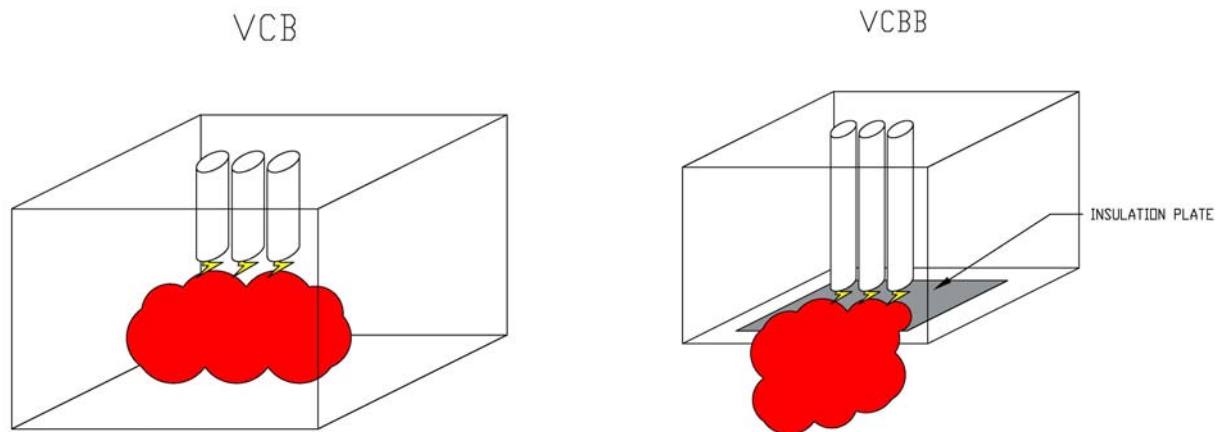


Figure 1 – Vertical Electrodes

In Figure 2, a horizontal arrangement of the three phases is illustrated with an arc flash at the end of the electrodes. This configuration is labeled as HCB. With the electrodes in a horizontal position, even more heat, i.e. incident energy, can be expelled out the front opening toward the person.

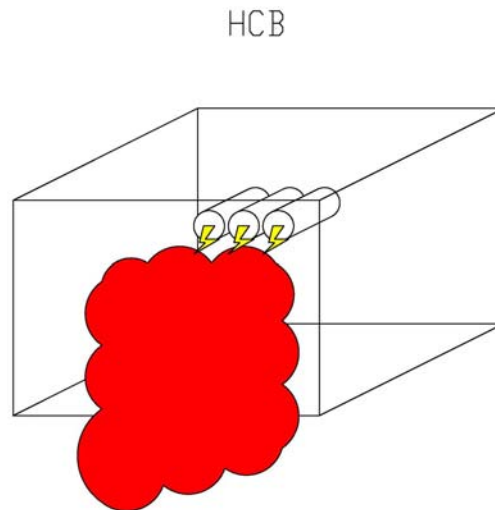


Figure 2 – Horizontal Electrode

IEEE Standard 1584-2018 provides the equations for making the incident energy calculations for these three configurations. The dimensions of the enclosure are also variables in the calculations. The result is that the new equations are more complex and require more information about the physical configuration of the equipment.

2.0 EXAMPLE

An example system is used to compare the equations in 1584-2002 with those in 1584-2018. It is setup with very specific parameters, but it does give a big-picture view of how the incident energy calculations can change. The calculations for the example system are given in Figures 3 thru 6 as follows:

- Figure 3 IEEE 1584-2002
- Figure 4 IEEE 1584-2018 VCB Configuration
- Figure 5 IEEE 1584-2018 VCBB Configuration
- Figure 6 IEEE 1584-2018 HCB Configuration

The results of the calculations are given in Tables 1 thru 3. The following observations are noted:

- In Table 1, the calculations are compared in calories/cm² at 13.8 kV and 480V.
- In Table 2, the calculations are given in % of the 1584-2002 methodology.
 - The VCB configuration gives results that are closest to the 1584-2002 methodology.
 - The VCBB configuration tends to give incident energies that are approximately 1.5 times the VCB calculations, except for the 480V panelboard and MCC equipment where the values are closer.
 - The HCB configuration tends to give incident energies that are approximately 2.0 times the VCB calculations.
- In Table 3, the calculations are summarized by PPE level where PPE = 2 is for incident energy values ≤ 8 cal/cm² and PPE = 4 is for values ≤ 40 cal/cm². The areas where a PPE level would change are noted in the table.

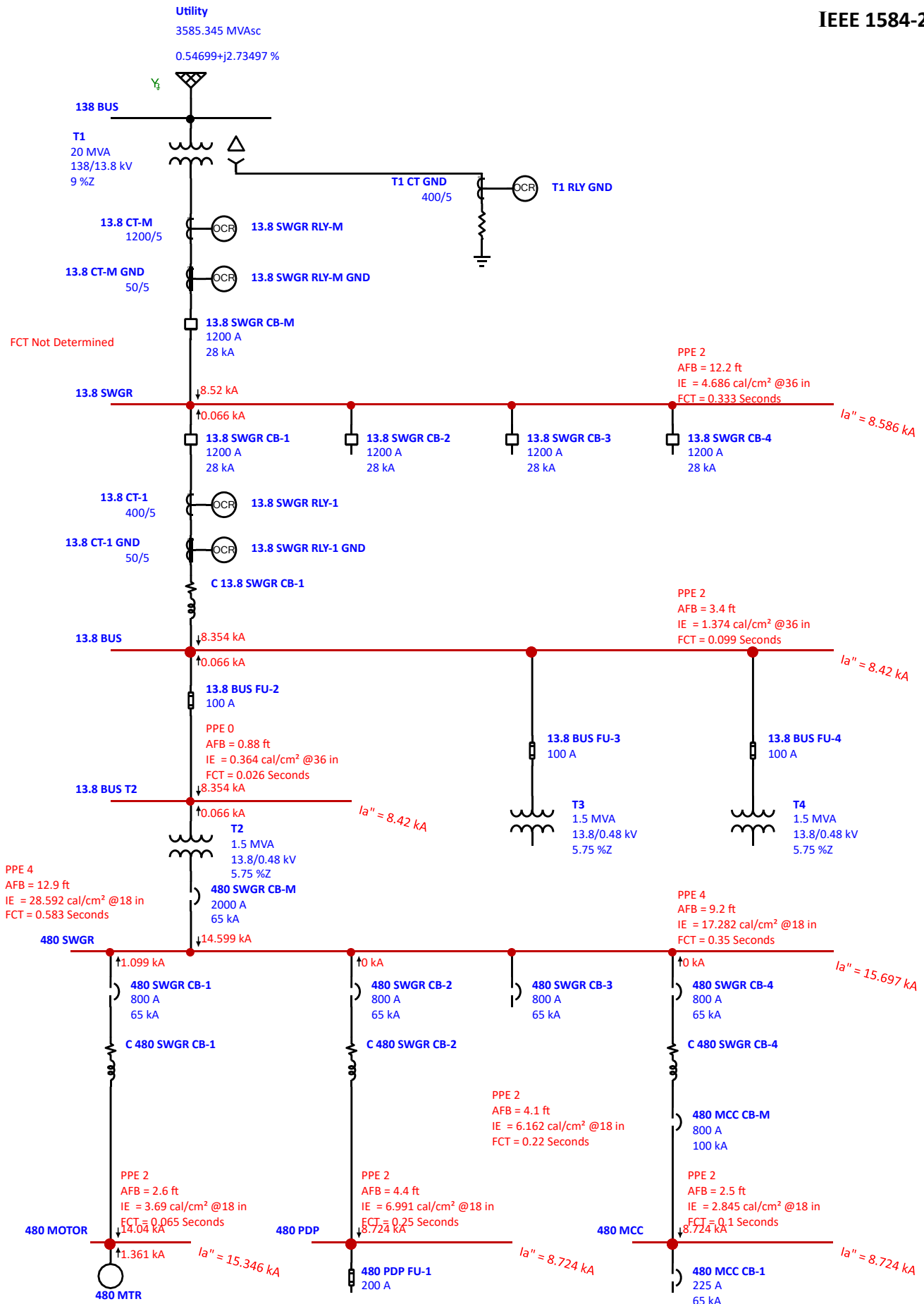


Figure 3

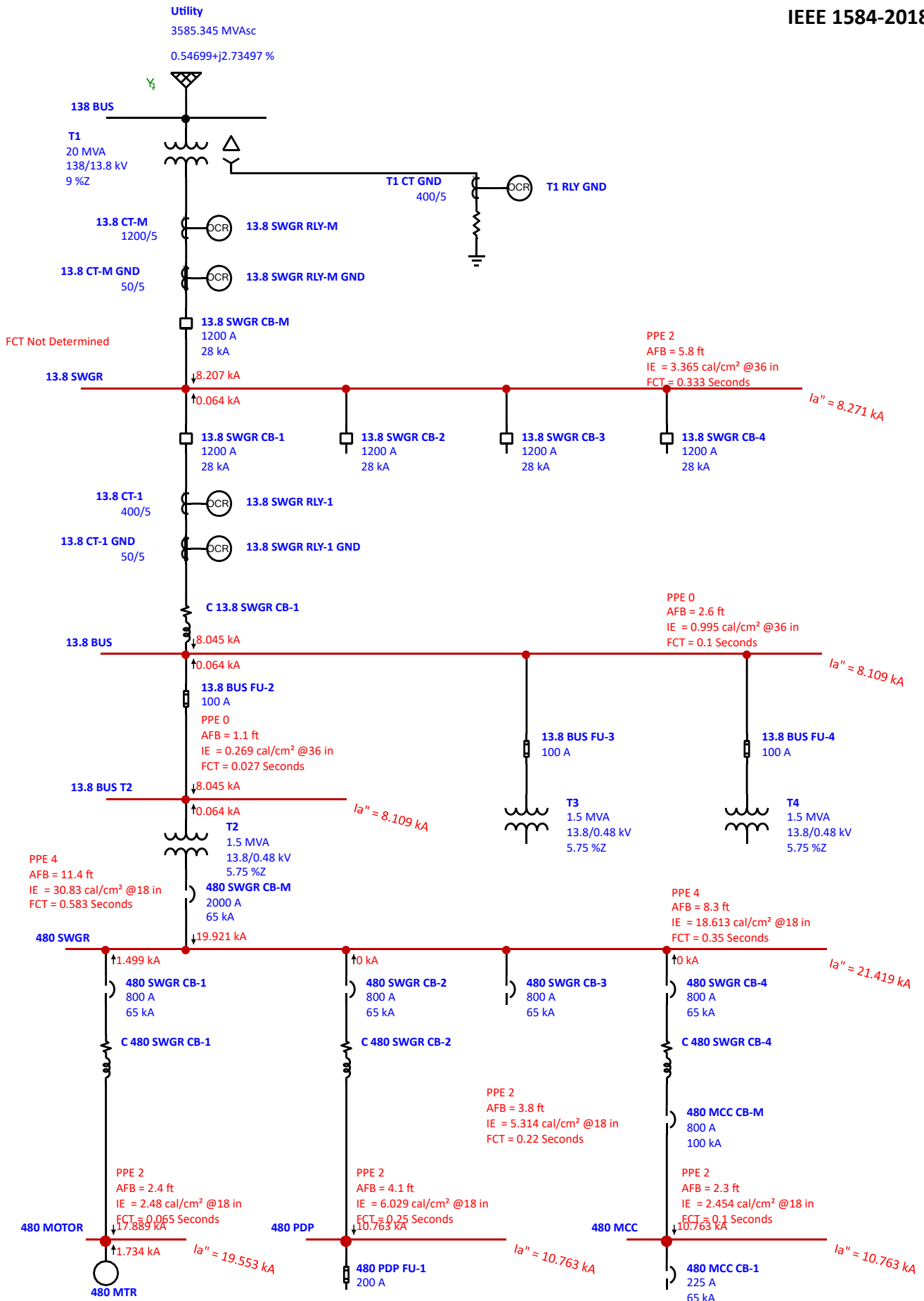


Figure 4

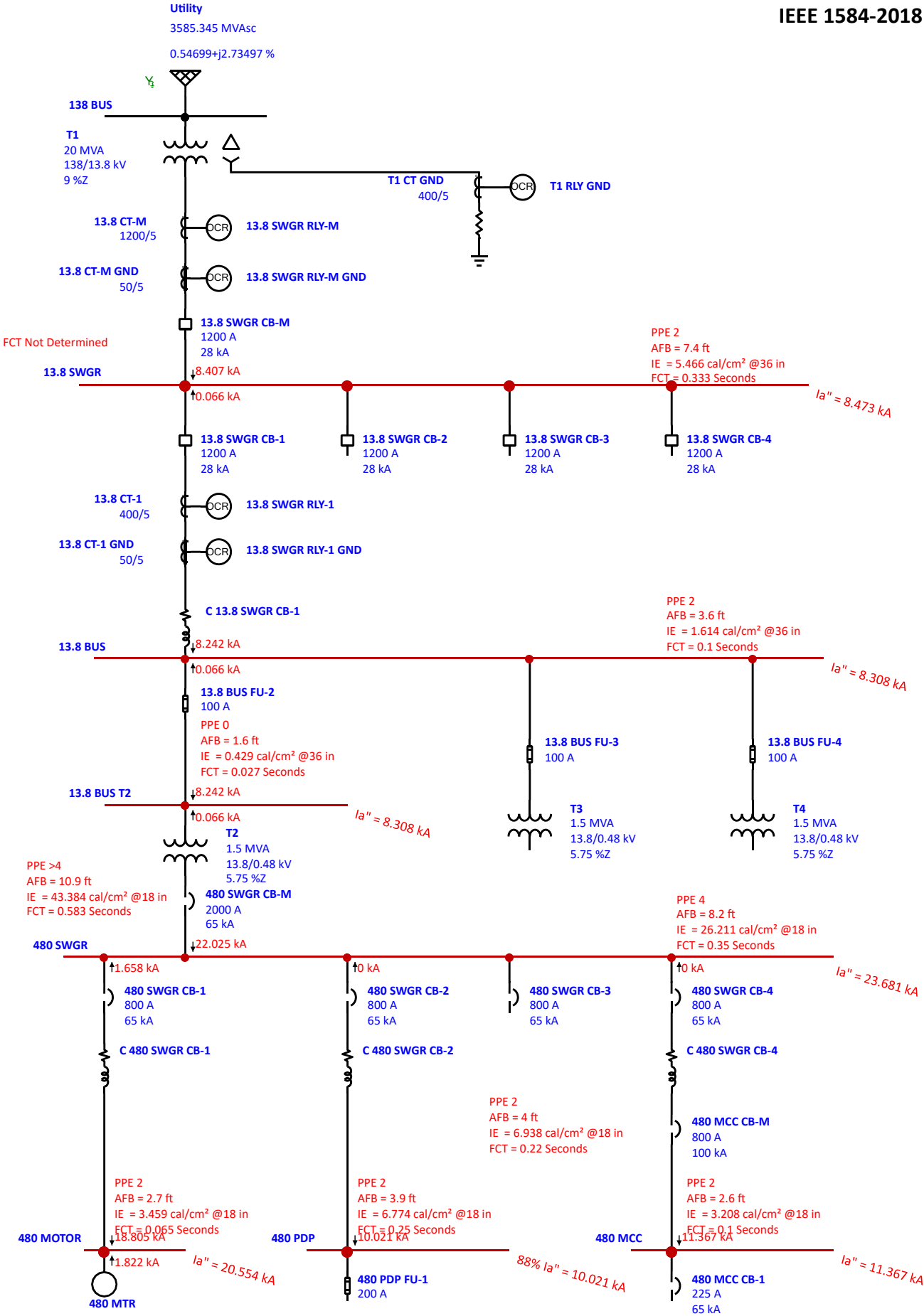


Figure 5

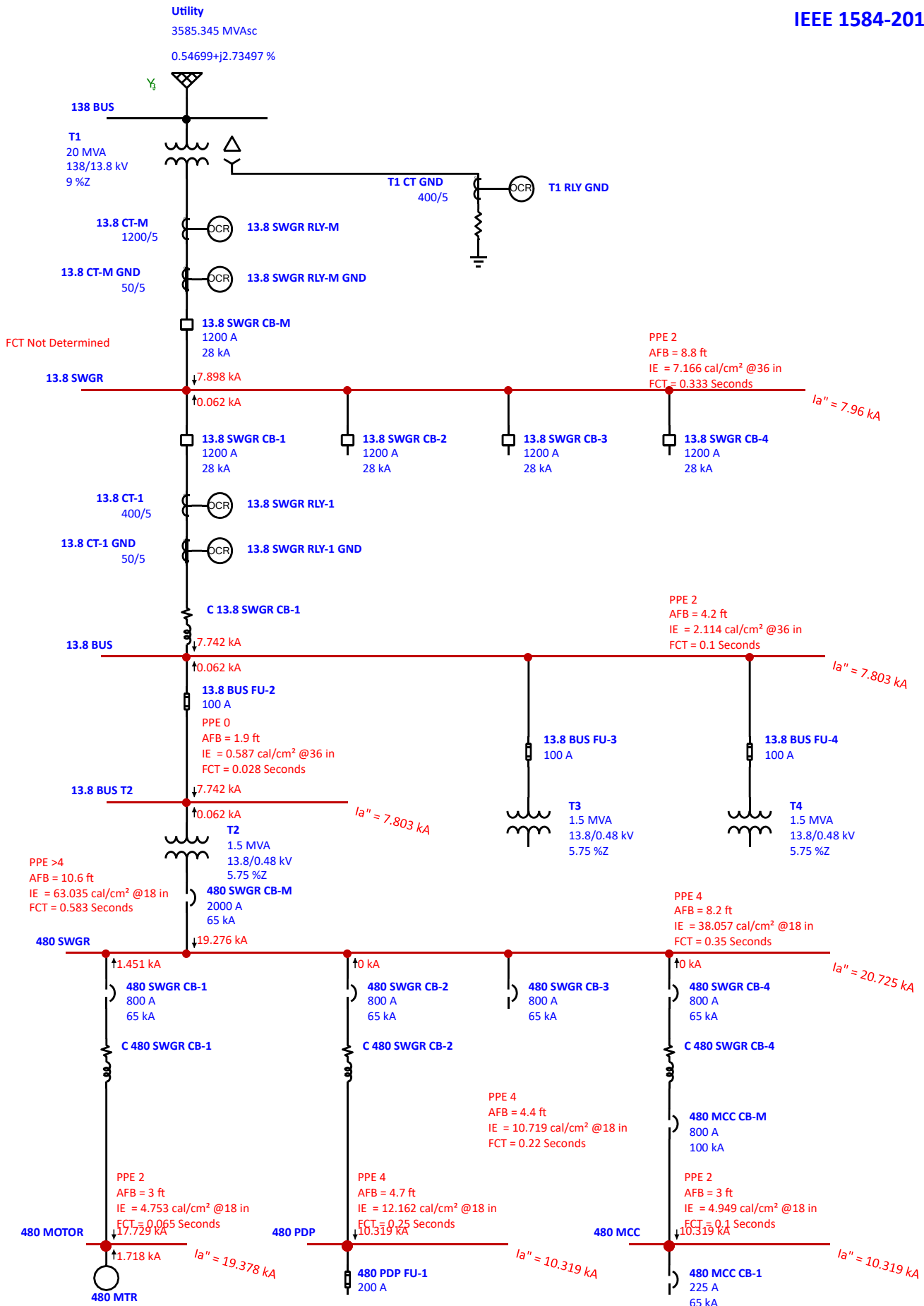


Figure 6

Table 1 - Comparison of Incident Energy Calculations

Bus	Voltage (kV)	Equipment Type	Working Distance (Inches)	Enclosure Dimensions (Inches)			Clearing Time (seconds)	Incident Energy (cal/cm ²)					
				H	x	W		x	D	2018			
										2002	VCB	VCBB	VCB
13.8 SWGR	13.8	Switchgear	36	45	30	30	0.33	4.7	3.4	5.5	7.2		
13.8 BUS	13.8	Switchgear	36	45	30	30	0.10	1.4	1.0	1.6	2.1		
13.8 BUS T2	13.8	Switchgear	36	45	30	30	0.03	0.4	0.3	0.4	0.6		
480 SWGR CB-M	0.48	LVCB	18	20	20	20	0.58	28.6	30.8	43.4	63.0		
480 SWGR	0.48	Switchgear	18	20	20	20	0.35	17.3	18.6	26.2	38.1		
480 MOTOR	0.48	Other	18	14	12	8	0.07	3.7	2.5	3.5	4.8		
480 PDP	0.48	Panelboard	18	14	12	8	0.25	7.0	6.0	6.8	12.2		
480 MCC	0.48	MCC	18	14	12	8	0.10	2.9	2.5	3.2	4.9		

Table 2 - Comparison of % of 2002 Calculation Method

Bus	Voltage (kV)	Equipment Type	Working Distance (Inches)	Enclosure Dimensions (Inches)			Clearing Time (seconds)	Incident Energy as % of 2002					
				H	x	W		x	D	2018			
										2002	VCB	VCBB	VCB
13.8 SWGR	13.8	Switchgear	36	45	30	30	0.33	100%	72%	117%	153%		
13.8 BUS	13.8	Switchgear	36	45	30	30	0.10	100%	73%	118%	154%		
13.8 BUS T2	13.8	Switchgear	36	45	30	30	0.03	100%	74%	118%	161%		
480 SWGR CB-M	0.48	LVCB	18	20	20	20	0.58	100%	108%	152%	220%		
480 SWGR	0.48	Switchgear	18	20	20	20	0.35	100%	108%	152%	220%		
480 MOTOR	0.48	Other	18	14	12	8	0.07	100%	67%	94%	129%		
480 PDP	0.48	Panelboard	18	14	12	8	0.25	100%	86%	97%	174%		
480 MCC	0.48	MCC	18	14	12	8	0.10	100%	86%	113%	174%		

Table 3 - Comparison of PPE Levels

Bus	Voltage (kV)	Equipment Type	Working Distance (Inches)	Enclosure Dimensions (Inches)			Clearing Time (seconds)	PPE Level (2 or 4)					
				H	x	W		x	D	2018			
										2002	VCB	VCBB	VCB
13.8 SWGR	13.8	Switchgear	36	45	30	30	0.33	2	2	2	2		
13.8 BUS	13.8	Switchgear	36	45	30	30	0.10	2	2	2	2		
13.8 BUS T2	13.8	Switchgear	36	45	30	30	0.03	2	2	2	2		
480 SWGR CB-M	0.48	LVCB	18	20	20	20	0.58	4	4	>4	>4		
480 SWGR	0.48	Switchgear	18	20	20	20	0.35	4	4	4	4		
480 MOTOR	0.48	Other	18	14	12	8	0.07	2	2	2	2		
480 PDP	0.48	Panelboard	18	14	12	8	0.25	2	2	2	4		
480 MCC	0.48	MCC	18	14	12	8	0.10	2	2	2	2		

This is a change in PPE from the 2002 calculation method.

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